General Disclaimer

One or more of the Following Statements may affect this Document

- This document has been reproduced from the best copy furnished by the organizational source. It is being released in the interest of making available as much information as possible.
- This document may contain data, which exceeds the sheet parameters. It was furnished in this condition by the organizational source and is the best copy available.
- This document may contain tone-on-tone or color graphs, charts and/or pictures, which have been reproduced in black and white.
- This document is paginated as submitted by the original source.
- Portions of this document are not fully legible due to the historical nature of some
 of the material. However, it is the best reproduction available from the original
 submission.

NASA Technical Memorandum

NASA TM-82544



DEVELOPMENT OF LOW VISCOSITY ALKANE-BASED URETHANE FOR CONNECTOR POTTING APPLICATIONS

By Donald E. Morris

July 1983

(NASA-TM-82544) DEVELOPMENT OF LOW VISCOSITY ALKANE-BASED URETHANE FOR CONNECTOR POTTING APPLICATIONS (NASA) 28 P HC A03/MF A01 CSCL 11G

N83-34047

Unclas 36067

G3/27

National Aeronautics and

Space Administration

George C. Marshall Space Flight Center

		TECHNIC	AL REPORT STANDARD TITLE PAGE
1, REPORT NO.	2. GOVERNMENT A	ACCESSION NO.	3. RECIPIENT'S CATALOG NO.
NASA TM-82544			
4. TITLE AND SUBTITLE	A. 1 12	ن سند ه	5, REPORT DATE
Development of Low Vis		ed Urethane for	July 1983
Connector Potting Appli	leations		6. PERFORMING ORGANIZATION CODE
	The state of the s		
7. AUTHOR(S)			B. PERFORMING ORGANIZATION REPORT #
Donald E. Morris			
9. PERFORMING ORGANIZATION NAME			10, WORK UNIT, NO.
George C. Marshall Spa			
Marshall Space Flight C	enter, Alabama 35	812	11, CONTRACT OR GRANT NO.
			13, TYPE OF REPORT & PERIOD COVERED
2. SPONSORING AGENCY NAME AND A		······································	7
National Aeronautics and	d Space Administr	ation	Technical Memorandum
Washington, D.C. 20546	}		
,			14, SPONSORING AGENCY CODE
			,,,,
15. SUPPLEMENTARY NOTES			
IOT SOLIEMINENIANI HAIES			
Prepared by Materials a	and Propagas Lahe	oratory Science	and Engineering
Frepared by materials a	mu Frocesses Labo	oratory, belefice	and Engineering
16, ABSTRACT			
			s were prepared with
			-cyclohexyl isocyanate). The
urethanes with molecula	r weights as grea	t as 2500 had vis	concition low anough and a
Caronical Viales Indaoodic	it Motering on Eron	- as	scosities low enough and a
working life long enoug	th to be used in p	otting, molding,	and coating applications.
working life long enoug Specimens were prepare	th to be used in ped and mechanical	otting, molding, properties such	and coating applications. as hardness, tensile strength
working life long enoug Specimens were prepare elongation, and tear str	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear stransition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear stransition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear str transition and expansion	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass
working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined.	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome thermogravimetr	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were
working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined.	th to be used in p ed and mechanical rength were deteri	otting, molding, properties such mined. Thermome	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were
Working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined. 17. KEY WORDS Urethane Tensile	th to be used in ped and mechanical rength were determined to coefficient) and	otting, molding, properties such mined. Thermome thermogravimetr	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were
Working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined. 17. KEY WORDS Urethane Tensile	th to be used in ped and mechanical rength were determined to coefficient) and	properties such mined. Thermome thermogravimetr	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were
Working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined. 17. KEY WORDS Urethane Tensile Alkane Tear St	th to be used in ped and mechanical rength were determent coefficient) and Strength trength	otting, molding, properties such mined. Thermome thermogravimetr	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were
working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined. IT. KEY WORDS Urethane Tensile Alkane Tear Stransition Thermo	sh to be used in ped and mechanical rength were determent coefficient) and strength trength benechanical	properties such mined. Thermome thermogravimetr	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were
working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined. IT. KEY WORDS Urethane Tensile Alkane Tear Stransition Thermo	th to be used in ped and mechanical rength were determent coefficient) and Strength trength	properties such mined. Thermome thermogravimetr	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were
working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined. IT. KEY WORDS Urethane Tensile Alkane Tear Stransition Thermo	sh to be used in ped and mechanical rength were determent coefficient) and strength trength benechanical	properties such mined. Thermome thermogravimetr	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were
working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined. IT. KEY WORDS Urethane Tensile Alkane Tear Stransition Thermo	sh to be used in ped and mechanical rength were determent coefficient) and strength trength benechanical	properties such mined. Thermome thermogravimetr	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were
working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined. 17. KEY WORDS Urethane Tensile Alkane Tear Stransition Thermo Viscosity Thermo	Strength trength mechanical and mechanical rength were determent coefficient) and strength trength mechanical agravimetric	properties such mined. Thermome thermogravimetr. 18. DISTRIBUTION ST. Unclassified	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were
working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined. 7. KEY WORDS Urethane Tensile Alkane Tear Stransition Thermo Viscosity Thermo	Strength trength were determined and mechanical rength were determined and strength trength trength procedures are also security classifications.	otting, molding, properties such mined. Thermome thermogravimetr. 18. DISTRIBUTION ST Unclassified	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were TATEMENT d-Unlimited
working life long enoug Specimens were prepare elongation, and tear stransition and expansion determined. 7. KEY WORDS Urethane Tensile Alkane Tear Stransition Thermo Viscosity Thermo	Strength trength mechanical and mechanical rength were determent coefficient) and strength trength mechanical agravimetric	otting, molding, properties such mined. Thermome thermogravimetr. 18. DISTRIBUTION ST Unclassified	and coating applications. as hardness, tensile strength echanical properties (glass ic properties were

ACKNOWLEDGMENTS

The author wishes to express appreciation to Dr. S. P. McManus, University of Alabama in Huntsville, and Dr. B. G. Penn, Polymers and Composites Branch, for suggestions incorporated into this study; and to Mr. L. M. Thompson and Mr. W. T. White, Polymers and Composites Branch, for assistance in the determination of tear and tensile strength and percent elongation.

This study was supported by the Center Director's Discretionary Fund and was reviewed and monitored by MSFC Discretionary Fund Advisory Panel chaired by Mr. T. J. Lee.

ORIGINAL PAGE 19' OF POOR QUALITY

TABLE OF CONTENTS

		Page
ı.	INTRODUCTION	1
II.	URETHANE PREPARATION	3
	A. Hydrogenation of Polybutadiene B. Alkane Diols C. Diisocyanates D. Curing Agents E. Preparation of Test Specimens	3 4 6 7 10
III.	URETHANE EVALUATION	1.1
	A. Hardness B. Tensile Strength and Elongation C. Tear Strength D. Glass Transition and Expansion Coefficient E. Thermogravimetric Analysis	11 11 13 14 16
ıv.	CONCLUSIONS	16
v.	BIBLIOGRAPHY	21

LIST OF ILLUSTRATIONS

Figure	Title	Page
1.	Infrared spectrum of hydroxy-terminated polybutadiene	4
2.	Infrared spectrum of hydrogenated, hydroxy-terminated polybutadiene	5
3.	Viscosity of catalyzed urethanes versus time	8
4.	Viscosity of alkane-based urethanes catalyzed for one hour versus molecular weight of diol	9
5.	Thermomechanical analysis of alkane-based urethane	15
6.	Weight loss of urethanes versus temperature	18
7.	Weight loss of alkane-based urethanes versus temperature	19

LIST OF TABLES

Table	Title	Page
1.	Characterization of Diols	6
2.	Composition of Alkane-Based Urethanes	10
3.	Hardness of Cured Urethanes	11
41.	Tensile Strength at Break, PSI	1,2
(5.	Elongation at Break, Percent	
6.	Tear Strength, LBS/IN	13
7.	Glass Transition, °C	14
8.	Expansion Coefficient, µ m/m-°C	15
9.	Thermogravimetric Analysis	17
10.	Comparison of Properties of Experimental Urethanes with Requirements of Specifications for Urethane Potting	20

DEVELOPMENT OF LOW VISCOSITY ALKANE-BASED URETHANE FOR CONNECTOR POTTING APPLICATIONS

I. INTRODUCTION

It was established in a previous Discretionary Fund task that alkane-based urethanes are hydrolytically and oxidatively stable and have excellent dielectric properties. However, the urethanes prepared from most commercially available alkane materials are very viscous liquids or semi-solids which cannot be easily used in potting applications. To take advantage of the inherently good properties of this type of urethane, this study has been directed toward the development of alkane-based urethanes with viscosities low enough to permit easy mixing with catalyst at room temperature, followed by out-gassing, and molding.

Polyurethanes are made essentially of three basic components: difunctional polyols, disocyanates, and chain extenders. It is the interaction of these three components which produces the polyurethane:

urethane prepolymer

The urethane is cured with chain extenders which in this study, consisted of a diamine.

Each of these components can influence the viscosity of the reaction mixture. Pot life, or time interval before the material is too viscous to use, will depend upon the relative reactivity of the components, the molecular weight, and the molecular structure,

Most of the alkane-based urethanes used in this study were prepared by the hydrogenation of hydroxy-terminated polybutadiene. The high viscosity of the resulting urethane is due to crystallinity and to the high molecular weight of the polybutadiene used. The preparation of hydroxy-terminated polybutadiene by anionic techniques lead to both 1,2- and 1,4- additions of butadiene:

One typical commercially available hydroxy-terminated polybutadiene is:

HO
$$CH = CH$$
 CH_2
 CH_2

The predominant configuration is trans-1,4 (60 percent) with approximately 20 percent each cis-1,4 and vinyl-1,2. Hydrogenation yields

$$\text{HO} = \left[\left(\text{CH}_2 \right) \right]_4 \quad \text{CH}_2 \quad \text{CH}_2 \quad \left(\text{CH}_2 \right) \quad \text{DH}_2 \quad \text{CH}_3 \quad \text{CH}_2 \quad \text{CH}_3 \quad \text{CH}_4 \quad \text{CH}_4 \quad \text{CH}_5 \quad \text{CH}$$

Hydrogenation of the 1,4-chain leads to polyethylene, a highly crystalline polymer, whereas, hydrogenation of the 1,2-chain would yield poly-1-butene, presumably atactic, and hence non crystalline. A study of methods for preparing polybutadiene with a high 1,2-addition content was not within the scope of this study. However, the range of usable molecular weights found by this study could undoubtably be extended by the use of highly branched polyols to disrupt the chain regularity

. 416 -

ORIGINAL PAGE IS

favoring crystallinity and thus lower the polymer viscosity. As an example, a urethane prepared from 1,12-dodecanediol, molecular weight 202, had an initial viscosity greater than 20,000 poise; while one prepared from a hydrogenated polybutadiene diol, molecular weight 1350, had an initial viscosity of 380 poise.

Seven alkane-based polyols, varying in molecular weight from approximately 300 to 4000, were used for preparing polyurethanes to be used in this study. With one exception, the polyols were prepared by the hydrogenation of hydroxy-terminated polybutadiene. Hydrogenated ricinoleic acid,

HO-CH-C₁₀
$$H_{20}$$
 CH_2 OH , C_6 H_{13}

was used as the lowest molecular weight diol.

Diisocyanates are the second group of components used in the manufacture of polyurethanes. These chemicals end-cap the polyols and supply the active sites necessary for cross-linking or chain extension. The most commonly used and least expensive diisocyanate is 2,4-toluene diisocyanate (TDI). However, in this study, two aliphatic diisocyanates, isophorone dissocyanate and methylene bis(4-cyclohexylisocyanate), were used to evaluate their effect on pot life as compared to the aromatic TDI-type diisocyanate.

The final component of polyurethanes is the chain-extender or cross-linker. This component allows the urethane prepolymer to reach its final molecular weight and converts it via crosslinks to a thermoset material. The chain extenders fall into two categories, diols and amines. Both types were used in this study. The most common diamine type is 4,4' methylene-bis(2-chloroaniline), known under the DuPont trade name MOCA. This curing agent adds toughness to the urethane; but it was not used in this study because it is a carcinogen suspect. Polacure 740M, trimethylene glycol di-p-aminobenzoate made by Polaroid Corporation, was used. 1,4-Butanediol was used in one series of urethanes.

Three series of urethanes with molecular weights from 300 to 4000 were prepared, molded, and cured into configurations for the evaulation of physical properties. The cured urethanes were tested for hardness, tensile and tear strength, percent elongation, and specific gravity. These properties were compared to that required by MSFC-SPEC-515, which is the controlling specification for urethane potting and molding material. Thermogravimetric and thermomechanical analyses were performed to further characterize these materials.

II. URETHANE PREPARATION

A. Hydrogenation of Polybutadiene

The polybutadiene diol was hydrogenated using a Parr 3921, shaker type, hydrogenation apparatus. A 200 W glass fabric heating mantle was used for heating the reaction bottle. The temperature of the reaction was automatically controlled with a Parr 3931 temperature controller and a stainless sheathed thermistor probe in the

reaction bottle.

One hundred grams of hydroxy-terminated polybutadiene was dissolved in 1 liter of toluene in a 2-liter reaction bottle. Approximately 1.0 gram of Palladium (5%) on activated carbon was added and the bottle was placed in the hydrogenation apparatus. The bottle was evacuated and refilled with nitrogen. This procedure was repeated three times. The vessel was evacuated and refilled with hydrogen twice. The apparatus was pressurized to 50 psig and the material reacted at 75°C. The reaction was allowed to proceed until a minimum of 90 percent of the theoretical amount of hydrogen was absorbed. The catalyst was then removed by Soxhlet extraction of the reaction mixture. The toluene was evaporated isolating the hydrogenated polybutadiene diol.

Figures 1 and 2 show the infrared spectrum of polybutadiene before and after hydrogenation. The disappearance of the absorption bands in the 910 cm⁻¹ to 1000 cm⁻¹ region, generally associated with cis, trans, and 1,2 vinyl units, indicates the polybutadiene has been hydrogenated. The groups were hydrogenated preferentially. The vinyl group was hydrogenated the most rapidly and the trans-1,4 the least. Some samples showed some residual unsaturated trans units. However, according to the amount of hydrogen absorbed, all samples were hydrogenated to 90 percent or greater.

B. Alkane Diols

The alkane diols used in this study were primarily hydrogenated, hydroxyterminated polybutadienes (HTPBD). Two of these materials under the trade name

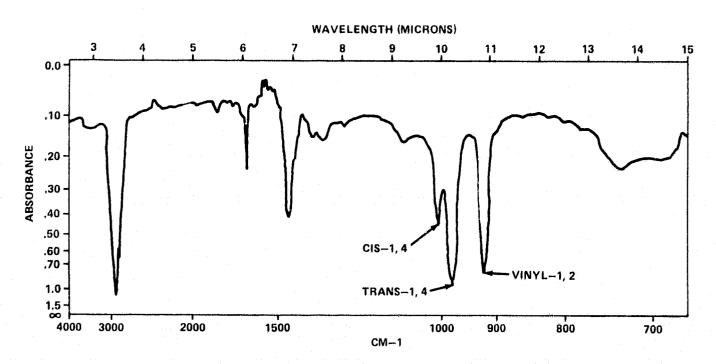


Figure 1. Infrared spectrum of hydroxy-terminated polybutadiene.

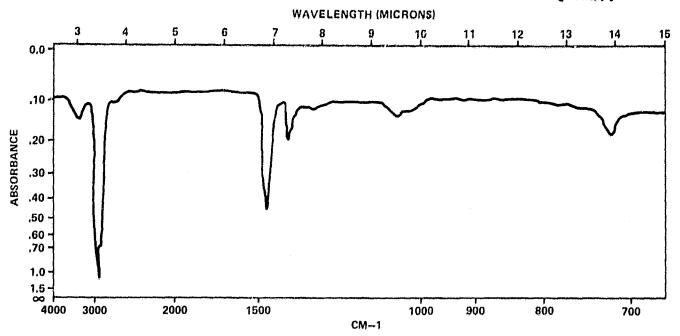


Figure 2. Infrared spectrum of hydrogenated, hydroxy-terminated polybutadiene.

Telagen-S were obtained from General Tire and Rubber Company. Hydroxy-terminated polybutadienes ranging in molecular weight from 450 to 3350 were obtained from Polyscience, LTD and Arco Chemical Company. This range would include and exceed the molecular weight required in the preparation of polyurethanes for connectorpotting applications.

Table 1 lists the diols used in this study. Molecular weights for those diols not furnished by the distributor were determined using gel permeation chromatographic (GPC) techniques. The chromatography studies were carried out on a Waters Associates liquid chromatograph equipped with a Model 6000 A solvent delivery system, Model 440 absorbance detector, and R 401 differential refractometer.

Hydroxyl functionality was calculated from hydroxyl number and number-average molecular weight. Hydroxyl number is the milligrams of OH expressed as potassium hydroxide per gram of sample. The hydroxyl equivalent weight is 1000 x molecular weight of potassium hydroxide/hydroxyl number or

Functionality of the diol is the number-average molecular weight/hydroxyl equivalent weight or

Functionality =
$$\frac{M_n \times Hydroxyl Number}{56.100}$$

ORIGINAL PAGE 13 OF POOR QUALITY

A functionality of two indicates two hydroxyl groups per molecule. Monofunctional molecules would prevent chain extension and result in a lower molecular weight of the cured polymer. The functionality of the diols used in this study was very close to two considering variations due to experimental error, with the exception of HTPBD 1350 and 2000 as indicated in Table 1. Mechanical properties of urethanes prepared from these diols would be suspect.

TABLE 1. CHARACTERIZATION OF DIOLS

	Molecular Weight Number Average,	
Alkane Diol	\overline{M}_{n}	Functionality
1,12-Dodecane diol	202	2.0
Hydrogenated Ricinoleic Acid	286	2.0
HTPBD 450	450	2.0
HTPBD 1350	1350	1.6
Telagen-S A595-88	1660	2.1
HTPBD 2000	2000	1.4
HTPBD 2800	2800	2.2
H'TPBD 3500	3350	2.3
Telagen-S 185M	3960	1.9

C. Diisocyanates

Two aliphatic disocyanates, isophorone disocyanate and methyl bis-(4-cyclohexylisocyanate), were studied in this project. Isophorone disocyanate or 3-isocyanate-methyl-3,5,5-trimethyl-cyclohexylisocyanate was obtained from Thorson Chemical Corporation. The structure is

$$\begin{array}{c|c} \text{CH}_3 \\ \hline \\ \text{CH}_3 \\ \hline \\ \text{CH}_2 \text{NCO} \\ \end{array}$$

Methyl-bis(4-cyclohexylisocyanate) was obtained from Mobay Chemical Corporation under the trade name Desmodur W. The structure is

ORIGINAL PAGE IS OF POOR QUALITY

Each disocyanate was used for preparing a series of urethanes with the diols in Table 1. The disocyanates react much more slowly with the diols than does TDI. Viscosity increases slowly resulting in a urethane with lower viscosity and a longer working life. Higher temperatures are required for complete cure. Because of lower reactivity some of these urethanes can be processed at elevated temperatures to take advantage of the resulting lower viscosities. A urethane prepared from 1,12-dodecanediol with a viscosity greater than 20,000 poise at room temperature was processed satisfactorily at elevated temperature. Viscosity decreases rapidly with increase in temperature. Some unique urethanes probably could be prepared by reacting these aliphatic disocyanates with phenol-type materials.

Relative reactivity of catalyzed urethanes prepared from the two aliphatic disocyanates and a commercial urethane of the TDI-type is illustrated in Figure 3. MSFC-SPEC-515, the specification for molding and potting material, requires that the application life of freshly mixed urethane (time for viscosity to exceed 1000 poise) should be at least 1 hr. The two experimental urethanes easily meet this requirement. The compassion of the application life of the three urethanes is:

Commercial urethane	1 to 2 hr	•
Isophorone urethane	2 to 3 hr	,
Desmodur W urethane	4 to 5 hr	,

However, the initial viscosity and the cure time of the two experimental diisocyanates exceed that required by MSFC-SPEC-515. Urethanes prepared from Desmodur W and hydrogenated, hydroxy-terminated polybutadienes of molecular weights up to 2500 (Fig. 4) are usable as potting and modling materials. Those prepared from isophorone diisocyanate are more viscous but are usable to about 2000 molecular weight. However, the urethanes have a high initial viscosity and a long cure time. These disadvantages must be weighed against the materials' excellent dielectric properties and moisture resistance.

D. Curing Agents

The urethanes were cured with trimethylene glycol di-p-aminobenzoate

$$H_2N - \left\langle \begin{array}{c} O \\ \parallel \\ - C - O - \left(CH_2 \right)_3 - O - C \\ \end{array} \right\rangle - NH_2$$

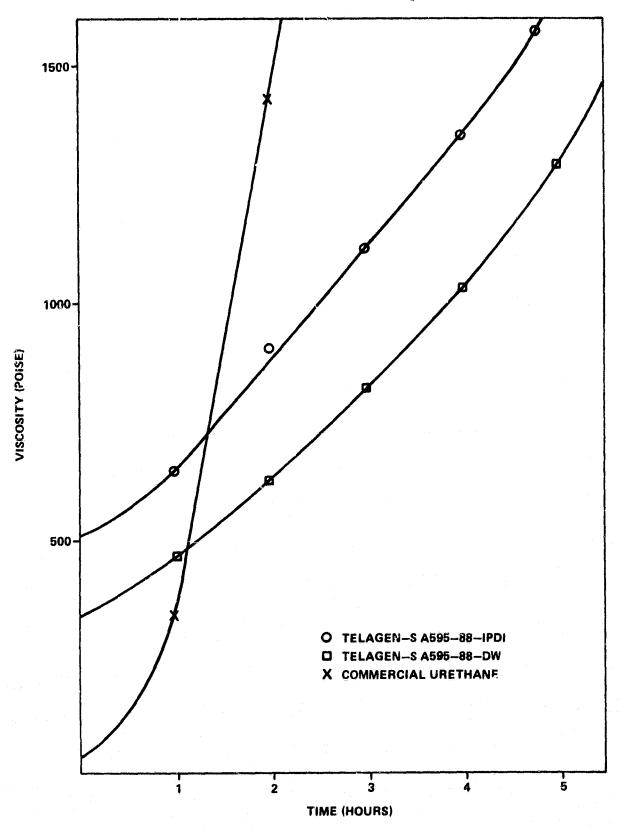


Figure 3. Viscosity of catalyzed urethanes versus time.

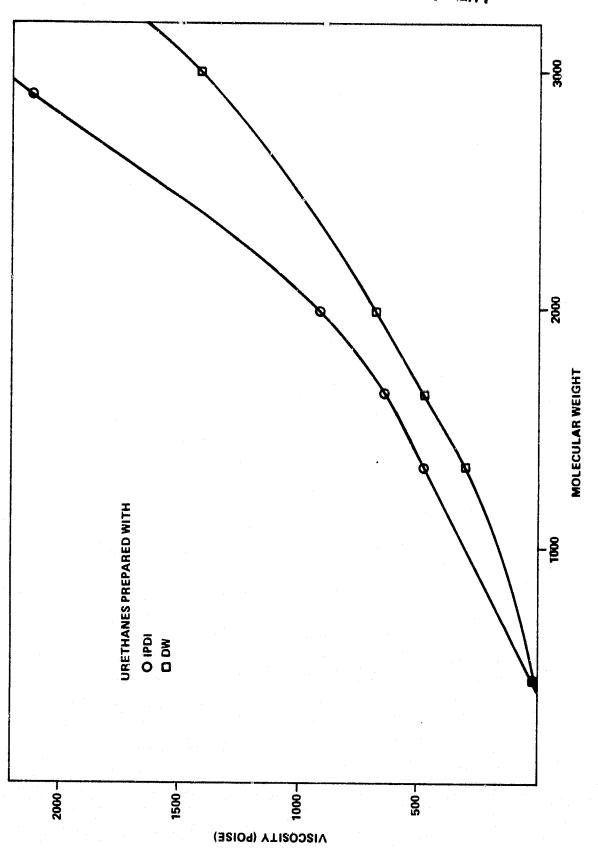


Figure 4. Viscosity of alkane-based urethanes catalyzed for one hour versus molecular weight of diol.

sold by Polaroid Corporation under the trade name Polacure 740M. Three series of urethanes were prepared with alkane diols listed in Table 2. One series was prepared with isophorone diisocyanate (IPDI) and one with Desmodur W (DW). These urethanes were cured with the Polacure 740M. One additional series was prepared with the alkane diols and isophorone diisocyanate and cured with a mixture of Polacure 740M and 1,4 butanediol to evaluate the diol as a chain extender.

TABLE 2. COMPOSITION OF ALKANE-BASED URETHANES

		Weight Diisccyanate g/100g		g Agents Og Diol
Alkane Diol	Diisocyanate	Diol	740M	Butanediol
Hydrogenated Ricinoleic Acid	IPDI	86.1	4.5	2.1
HTPBD 450	IPDI	64.5	4.2	3.8
HTPBD 1350	IPDI	33.0	4.2	4.3
Telagen-S A595-88	IPDI	26.8	4.0	3.1
HTPBD 2000	IPDI	22.2	3.8	2.3
HTPBD 2800	IPDI	15.8	3.6	1.1
HTPBD 3500	IPDI	13.2	3.6	0.6
Telagen-S 185M	IPDI	11.2	3.5	0.3
1,12 Dodecandiol	IPDI	117.4	5.4	
Hydrogenated Ricinoleic Acid	IPDI	80.4	- 4.2	-
HTPBD 450	IPDI	54.4	3.4	_
HTPBD 1350	IPDI	20.0	2.5	
Telagen-S A595-88	IPDI	16.9	2.5	-
HTPBD 2000	IPDI	14.7	2.5	_
HTPBD 2800	IPDi	11.7	2.7	
HTPBD 3500	IPDI	10.6	2.9	-
Telagen-S 185M	IPDI	10.0	3.1	_
1,12 Dodecandiol	DW	139.8	6.1	
Hydrogenated Ricinoleic Acid	DW	95.8	4.7	
HTPBD 450	DW	64.8	3.8	-
HTPBD 1350	DW	23.9	2.7	
Telagen-S A595-88	DW	20.2	2.6	-
HTPBD 2000	DW	17.5	2.7	-
HTPBD 2800	DW	14.0	2.8	-
HTPBD 3500	DW	12.8	3.0	
Telagen-S 185M	DW	12.0	3.2	-

E. Preparation of Test Specimens

The urethanes were prepared in a one step reaction with the alkane diol, diisocyanate, and chain extenders in the ratios shown in Table 2. Polacure 740M was dissolved by heating with the alkane diol. The diisocyanate was added to the mixture, stirred thoroughly, and then degassed. The reaction mixture was poured into molds for sheet material. The material was cured in air at 70°C for 12 hr and 120°C for

18 hr. Specimens for tensile strength, elongation, tear strength, and thermal tests were cut from the cured sheets of the elastomer for evaluation of mechanical properties.

III. URETHANE EVALUATION

A. Hardness

Hardness was measured with a Shore Durometer, Type A-2, with the exception of the urethanes prepared from 1,12-dodecanediol. Hardness for these urethanes was measured with Shore Durometer, Type D. The dodecanediol-urethane has a relatively short flexible chain and a very regular structure resulting in a highly crystalline and hard urethane. These urethanes are not elastomeric and are not suitable for potting applications. MSFC-SPEC-515 permits a hardness range of 60 to 90 Shore A hardness for potting applications. Most of the urethanes prepared in this study, as shown in Table 3, fall in this range.

B. Tensile Strength and Elongation

Tensile strength and elongation testing was in accordance with ASTM D 638-77. This method covers the determination of the tensile properties of plastics in the form of standard dumbell-shaped test specimens. The specimens were cut from cast sheets of the cured urethane. The values obtained for the experimental urethanes are shown in Tables 4 and 5. Urethanes prepared with Desmodur W have higher tensile strength

TABLE 3. HARDNESS OF CURED URETHANES

	Diisocyanate			
Alkane Diol	Desmodur W	Isophorone Diisocyanate	Isophorone ^a . Diisocyanate	
1,12-Dodecane Diol	78 D	78 D	-	
Hydrogenated Ricinoleic Acid	96	95	95	
HTPBD 450	77	83	89	
HTPBD 1350	67	63	76	
Telagen-S A595-88	64	60	74	
HTPBD 2000	64	62	73	
HTPBD 2800	64	61	72	
HTPBD 3500	64	63	60	
Telagen-S 185M	57	60	60	

a. 1,4 Butanediol added as chain extender as shown in Table 2.

TABLE 4. TENSILE STRENGTH AT BREAK, PSI

1	Diisocyanate			
Alkane Diol	Desmodur W	Isophorone Diisocyanate	Isophorone ^a . Diisocyanate	
1,12-Dodecane Diol	7510	8099		
Hydrogenated Ricinoleic Acid	2971	1600	2576	
HTPBD 450	629	516	892	
HTPBD 1350	320	294	339	
Telagen-S A595-88	729	523	729	
HTPBD 2000	383	358	390	
HTPBD 2800	656	405	806	
HTPBD 3500	445	408	458	

a. 1,4 Butanediol added as chain extender as shown in Table 2.

TABLE 5. ELONGATION AT BREAK, PERCENT

	Diisocyanate			
Alkane Diol	Desmodur W	Isophorone Diisocyanate	Isophorone ^a . Diisocyanate	
1,12-Dodecane Diol	70	90	-	
Hydrogenated Ricinoleic Acid	142	172	98	
HTPBD 450	167	172	182	
HTPBD 1350	192	243	197	
Telagen-S A595-88	437	525	275	
HTPBD 2000	74	83	142	
HTPBD 2800	125	175	170	
HTPBD 3500	192	197	155	

a. 1,4 Butanediol added as chain extender as shown in Table 2.

ORIGINAL PAGE IS OF POOR QUALITY

ORIGINAL PAGE TO OF POOR OUALITY

and lower percent elongation than those prepared with isophorene diisocyanate. The tensile strength of the isophorone diiscoyanate material was increased by the addition of 1,4 butanediol as a chain extender. A study directed toward cure optimization would probably result in urethanes with better mechanical properties but such a study is beyond the scope of this task.

MSFC-SPEC-515 requires a minimum 1500 psi tensile strength and 200 percent elongation for potting applications. The urethanes prepared from 1,12 dodecanediol has a very high tensile strength, but the material is not elastomeric, as indicated by its low percent elongation, and is not suitable for potting applications. The low values for tensile strength obtained for HTPBD 1350 and 2000 are probably due to their low functionality. Most of the experimental resins are usable as potting material. However, the alkane-based urethanes, in general are less elastomeric, more plastic, and not as tough as the ether-based urethane.

C. Tear Strength

Tear strength was determined in accordance with ASTM D624-54. The test specimens were cut with a Model C die from cast sheets of the cured urethane. Urethanes prepared with Desmodur W (Table 6) have slightly greater tear strength than those prepared with isophorone diisocyanate. The use of 1,4 butanediol with the isophorone diisocyanate as a chain extends improves the tear strength slightly. Hydroxy-terminated polybutadiene 2800, with a low functionality, formed urethanes with low tear strengths for all three formulations. MSFC-SPEC-515 requires a minimum tear strength of 175 lb/in. Most of these experimental urethanes do not meet these requirements. In general, the alkane-based urethanes are not as resistant to tear as are the ether-based materials.

TABLE 6. TEAR STRENGTH, LBS/IN

	Diisocyanate			
Alkane Diol	Desmodur W	Isophorone Diisocyanate	Isophorone a. Diisocyanate	
1,12-Dodecane Diol	1099	1096		
Hydrogenated Ricinoleic Acid	419	126	434	
HTPBD 450	72	63	83	
HTPBD 1350	69	65	69	
Telagen-S A595-88	112	93	119	
HTPBD 2000	62	52	58	
HTPBD 2800	109	97	126	
HTPBD 3500	97	95	100	

a. 1,4 Butanediol added as chain extender as shown in Table 2.

D. Glass Transition and Expansion Coefficient

Glass transitions and expansion coefficients for the experimental urethanes were determined with DuPont 943 Thermomechanical Analyzer in conjunction with the Dupont 1090 Thermal Analysis/Data System. Figure 5, a typical thermomechanical analysis of a an alkane-based urethane, shows the glass transition (T_g) of the material as well as coefficient of expansion (a) below and above T_g . Table 7 lists the glass transition temperatures for the experimental urethanes. Table 8 lists the expansion coefficients. The coefficient of linear thermal expansion is a very important parameter for materials used for coating circuit boards. It is possible for a thick coating with a high expansion coefficient to break a solder joint. MSFC-SPEC-507, specification for conformal coeting material for printed circuit boards, requires a maximum coefficient of expagision of 175µm/m °C from -55 to 100°C. As shown in Table 8, the expansion coefficient for a urethane below T_{g} is much less than that above T_{g} . This temperature range spans the glass transition range of most urethanes and includes two distinct rates of expansion. As a result the expansion rate over the specified range would be an average or resultant vector for the above Tg and below Tg rates. This is illustrated in Figure 5. The expansion coefficient is $75\mu\,\text{m/m}$ °C below $T_{\mbox{\scriptsize g}}$ and $338\mu m/m$ °C above T_{g} . It is $214\mu m/m$ °C between -55 and 100°C. The urethanes with the higher glass transition temperatures give the better expansion coefficients in the required range. In general, the alkane-based urethanes have expansion coefficients higher than is desirable for coating applications.

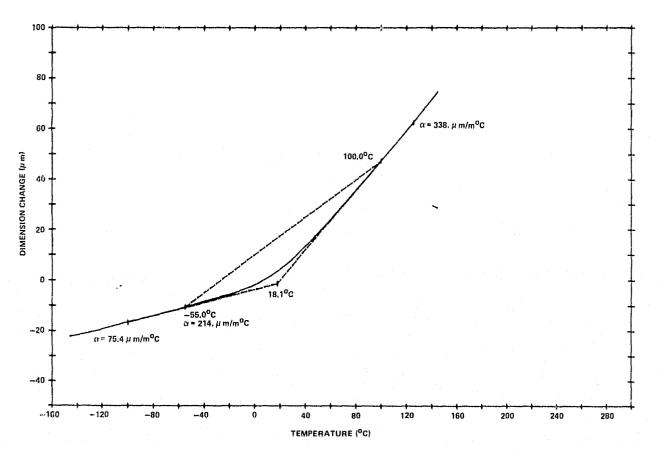


Figure 5. Thermomechancial analysis of alkane-based urethane.

TABLE 7. GLASS TRANSITION, °C

	Diisocyanate			
Alkane Diol	Desmodur W	Isophorone Diisocyanate	Isophorone ^a Diisocyanate	
1,12-Dodecane Diol	50	51,	-	
Hydrogenated Ricinoleic Acid	49	42	54	
HTPBD 450	17	15	19	
Telagen-S A595-88	-20	-16	-25	
HTPBD 2800	-9	-18	-17	
HTPBD 3500	-24	-19	-34	

a. 1,4 Butanediol added as chain extender as shown in Table 2.

TABLE 8. EXPANSION COEFFICIENT, µm/m °C

			Diisocya	nate		
	Desmo	dur W		orone yanate	Isopho Diisoc	rone ^a . yanate
Alkane Diol	Below T _g	Above T _g	Below T	Above T _g	Below T _g	Above T _g
1,12-Dodecane Diol	83	192	68	332		
Hydrogenated Ricinoleic Acid	118	207	136	232	111	246
HTPBD 450	132	263	129	305	75	337
Telagen-S A595-88	108	309	87	452	94	292
HTPBD 2800	139	405	115	325	112	330
HTPBD 3500	112	382	125	411	113	413

A. 1,4 Butanediol added as chain extender as shown in Table 2.

E. Thermogravimetric Analysis

Decomposition temperatures and weight loss for the alkane-base urethane were determined with a DuPont 951 Thermogravimetric Analyzer in conjunction with a DuPont 1090 Thermal Analysis/Data System. Table 9 summarizes the thermogravimetric analyses of the experimental alkane-based urethanes. The urethanes were heated to 600°C at a rate of 20 deg/min in gaseous nitrogen. Decomposition was almost complete for all samples. The temperature of onset of decomposition, the inflection point, and percent weight loss are shown in Table 9 for the three series of urethanes. The thermal stability of the experimental urethanes compare favorably with other urethane types shown in Figure 6. There is very little difference among the urethane types with the exception of the polybutadiene-based urethane. This urethane has a lower on-set temperature and appears to have two transition temperatures. The thermal stability of the three series of urethanes prepared in this study are very similar. Figure 7 compares three alkane-based urethanes prepared from hydrogenated ricinoleic acid (HRA). One urethane is prepared from ricinolic acid and Desmodur W (DW-HRA), one from the acid and isophorone diisocyanate (IPDI-HRA), and one with 1,4 butanediol added as a chain extender (IPDI-HRABA). The urethane prepared with Desmodur W appears to have the best thermal properties. The two prepared with isophorone diisocyanate have very similar properties. In general, the thermal properties of the alkane-based urethanes are comparable to other type urethanes.

IV. CONCLUSIONS

Alkane-based urethanes were prepared by reaction of both isophorone disocyanate and methyl-bis(4-cyclohexylisocyanate) with hydrogenated, hydroxytermianted polybutadiene. Urethanes with molecular weights up to 2500 had viscosities low enough to be used in potting and molding applications. Since the reactivity of the alkane disocyanates was less than that of their aromatic disocyanate counterparts, the working life of the experimental urethanes was longer than that of the average commercial urethane. However, the initial viscosity was higher. The higher molecular weight alkane-based urethanes were not suitable for potting applications. A comparison of the properties of the experimental urethanes with MSFC-SPEC 515 requirements is shown in Table 10.

The experimental urethanes could be prepared in the required hardness range, 60 to 90 Shore A. However, none of the urethanes met all of the requirements relating to hardness, tensile strength, elongation, and tear strength. The alkane-based urethanes did not have as high tensile strength, percent elongation, and resistance to tear as ether or ester-based urethanes. The experimental urethanes were less elastomeric, more plastic, and not as tough as ether-based material.

The thermal stability of the experimental urethanes was as good or better than ether, ester, and polybutadiene-based urethanes. The coefficient of linear thermal expansion for the material was higher than desirable for printed circuit board coatings.

The alkane-based urethane can be used for potting and molding applications. Up to 2500 molecular weight, viscosity is low enough and working life is long enough for this usage. Dielectric properties and hydrolytic stability are excellent. However, mechanical properties are not as good as those of ether and ester-based urethanes.

			Diisoc	Diisocyanate					
		Desmodur W			Isophorone Diisocyanate	a, 0)	Isc Di	Isophorone ^{a.} Diisocyanate	
Alkane Diol	Onset,	Inflection Point, °C	Weight Loss Percent	Onset,	Inflection Point, °C	Weight Loss, Percent	Onset, °C	Inflection Point, °C	Weight Loss, Percent
1.12-Dodecane Diol	359	393	95	356	387	26	-	1	ı
Hydrogenated Ricinoleic Acid	342	464	86	328	375	66	334	424	86
HTPBD 450	317	480	96	325	457	93	326	484	96
HTPBD 1350	342	446	97	340	422	L'ô	335	420	86
Telagen-S A595-88	359	453	26	350	468	66	339	468	66
HTPBD 2800	325	463	94	350	460	96	313	487	96
HTPBD 3500	375	482	66	380	464	96	325	479	96

a. 1,4 Butanediol added as chain extender as shown in Table 2.

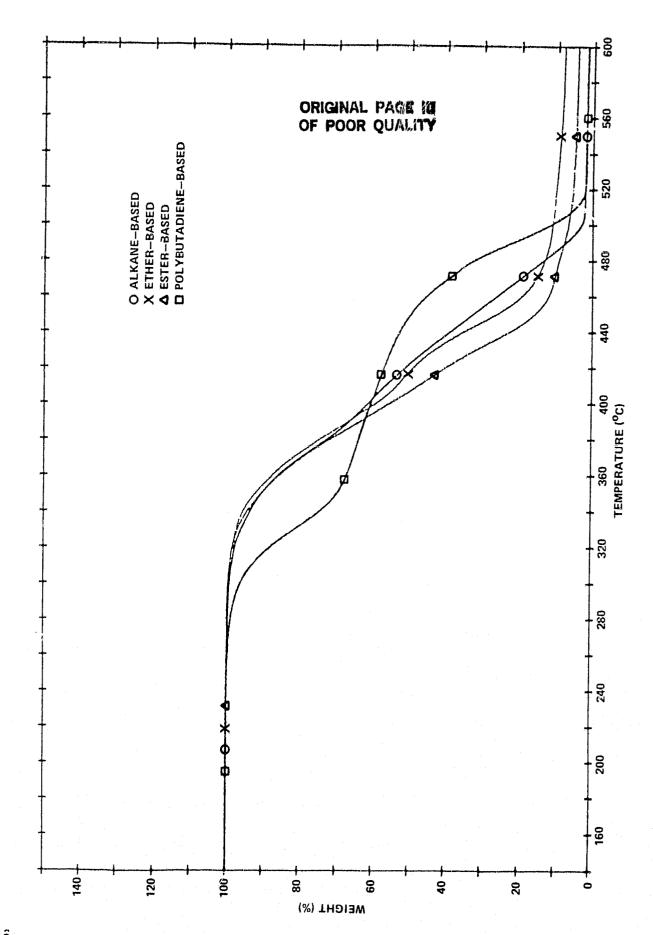
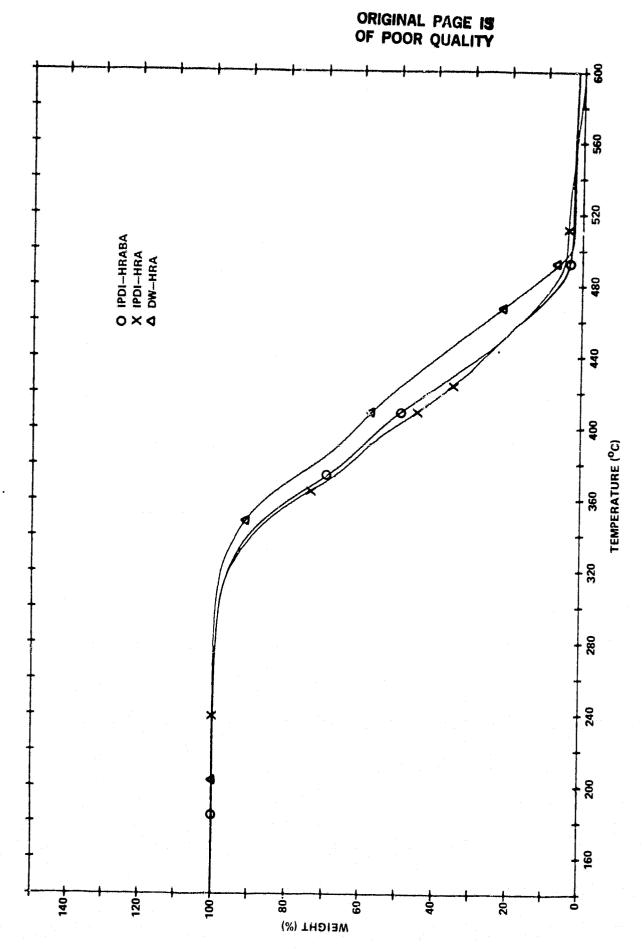


Figure 6. Weight loss of urethanes versus temperature.



Weight loss of alkane-based urethanes versus temperature. Figure 7.

TABLE 10. COMPARISON OF PROPERTIES OF EXPERIMENTAL UNTHANES WITH REQUIREMENTS OF SPECIFICATIONS FOR URETHANE POTTING MATERIAL

Properties	MSFC-SPEC	Experimental Alkane-Based Urethanes
Hardness, Shore A	60-90	57-96
Tensile Strength, psi	1500 min	400-3000
Tear Strength, lb/in	175 min	52-434
Elongation, percent	200 min	74-525
Viscosity, Initial at 25°C, poise	450 max	20-500
Application Life At 25°C, hours	1 min	2-10
Coefficient of Thermal Expansion, -55°C to +100°C, in/in/°C	175×10 ⁻⁶ max	162-324×10 ⁻⁶

a. Specification for urethane potting and molding elastomers.

BIBLIOGRAPHY

- Hendrickson, J. B., Cram, D. J., Hammond, G. S.: Organic Chemistry. McGraw-Hill Inc., New York, N.Y., 1970.
- MacKnight, W. J.: Studies of Polyurethanes and Epoxy Curing Reactions. University of Massachusetts, Final Report AMMRCTR 80-43, October, 1979.
- Moscanin, J., Eisenberg, A., Cuddihy, E. F.: On the Presence of Crystallinity in Hydrogenated Polybutadienes. NASA Technical Report 32-1512, September, 1970.
- Morris, D. E.: Development of Urethane Coatings and Potting Material with Improved Hydrolytic and Oxidative Stability. NASA Technical Memorandum, NASA-TM-82408, March, 1981.
- Ryan, P. W.: Urethane Elastomers Based on Hydroxyl Terminated Polybutadienes. Journal Elastoplastic, Vol. 3, p. 57, January, 1971.
 - Schollenberger, C. S., Stewart, F. D.: Thermoplastic Polyurethane Hydrolysis Stability. Journal Elastoplastics, Vol. 3, p. 28, January, 1971.
 - Webster, J. A.: Improved Potting and Encapsulating Compounds for Space Applications. Monsanto Research Corporation, Final Report NASS-21318, June, 1970.